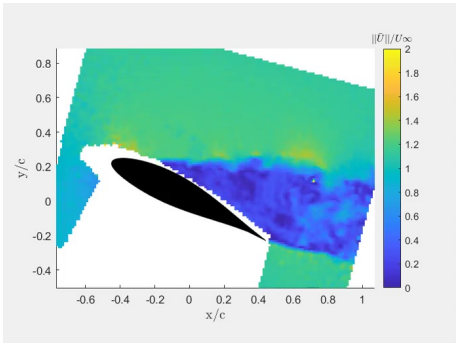


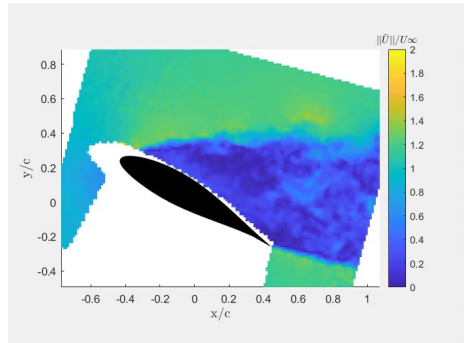
# Results for a static airfoil : flow topology

Absolute value of the normalized velocity  $\|\underline{U}\|/U_\infty$

$$\alpha_e = 23.8^\circ$$



$$\alpha_e = 26.3^\circ$$



We define the projected Strouhal number as :

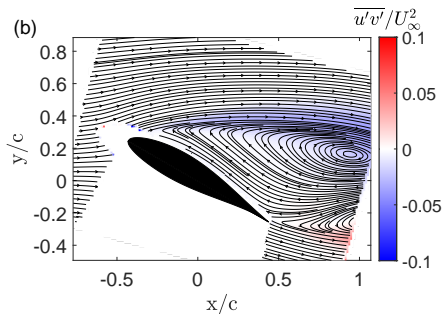
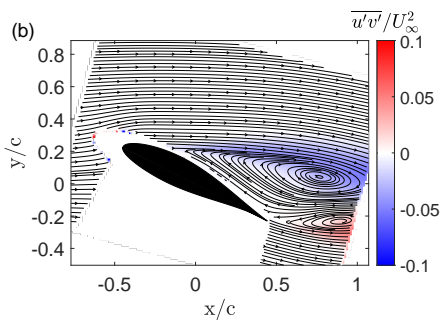
$$St = fL_{sep} \sin \alpha_e / U_\infty \quad \text{with} \quad L_{sep} \approx \begin{cases} 3c/4 & \text{for } \alpha_e = 23.8^\circ \\ c & \text{for } \alpha_e = 26.3^\circ \end{cases}$$

# Results for a static airfoil : flow topology

Streamlines of the mean flow and  $\overline{u'v'}$  component of the Reynolds tensor averaged over 10 runs

$$\alpha_e = 23.8^\circ$$

$$\alpha_e = 26.3^\circ$$

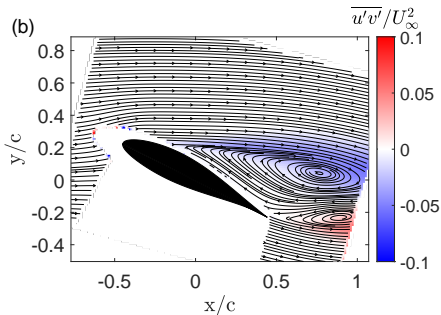


We define the projected Strouhal number as :

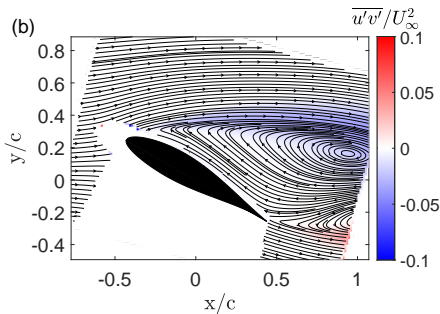
$$St = fL_{sep} \sin \alpha_e / U_\infty \quad \text{with} \quad L_{sep} \approx \begin{cases} 3c/4 & \text{for } \alpha_e = 23.8^\circ \\ c & \text{for } \alpha_e = 26.3^\circ \end{cases}$$

# Results for a static airfoil : flow topology

$$\alpha_e = 23.8^\circ$$



$$\alpha_e = 26.3^\circ$$



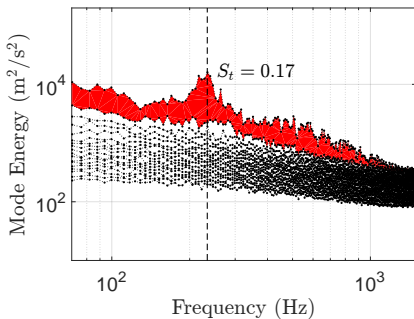
We define the projected Strouhal number as :

$$St = fL_{sep} \sin \alpha_e / U_\infty \quad \text{with} \quad L_{sep} \approx \begin{cases} 3c/4 & \text{for } \alpha_e = 23.8^\circ \\ c & \text{for } \alpha_e = 26.3^\circ \end{cases}$$

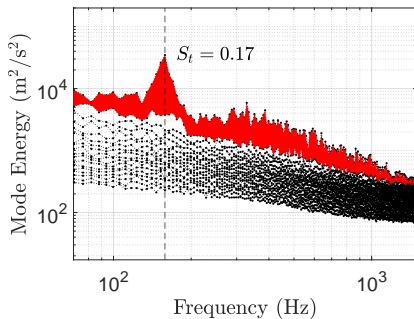
# Spectral Proper Orthogonal Decomposition

$$\hat{\mathbf{u}}(\mathbf{x}, f) = \sum_{j=1}^{\infty} a_j(f) \psi_j(\mathbf{x}, f) \quad \text{with} \quad \begin{cases} a_j : \text{expansion coefficient} \\ \psi_j : \text{SPOD mode} \end{cases}$$

$$\alpha_e = 23.8^\circ$$



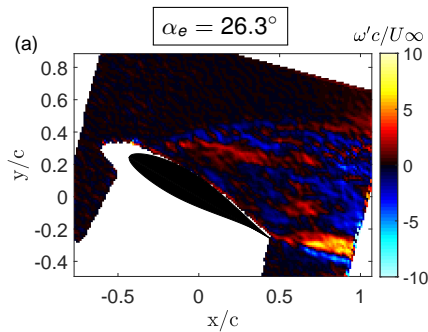
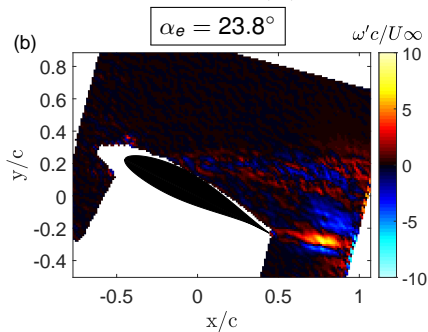
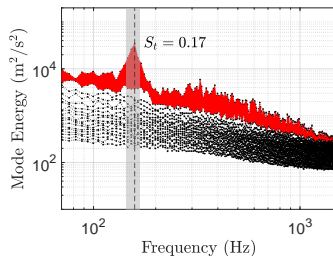
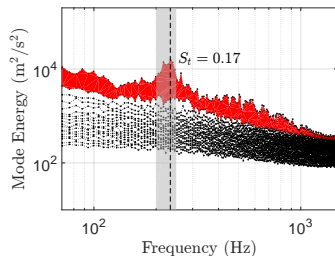
$$\alpha_e = 26.3^\circ$$



Low-rank behaviour over a wide range of frequency



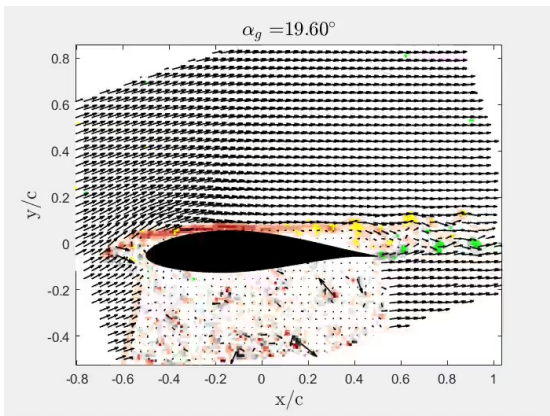
# Spectral Proper Orthogonal Decomposition



# Flow topology for $k = 0.005$ (quasi-static regime)

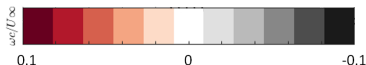
## Vortex detection criterion $\Gamma_2$

$$\Gamma_2(P) = \frac{1}{N} \sum_S \frac{[\underline{PM} \wedge (\underline{U}_M - \underline{U}_P)] \cdot \underline{z}}{\|\underline{PM}\| \cdot \|\underline{U}_M - \underline{U}_P\|} \quad \text{with } N = 3$$



## Flow evolution in the **airfoil reference system**

- 1) Streamlines
- 2) Normalized vorticity  $\omega c / U_\infty$  :



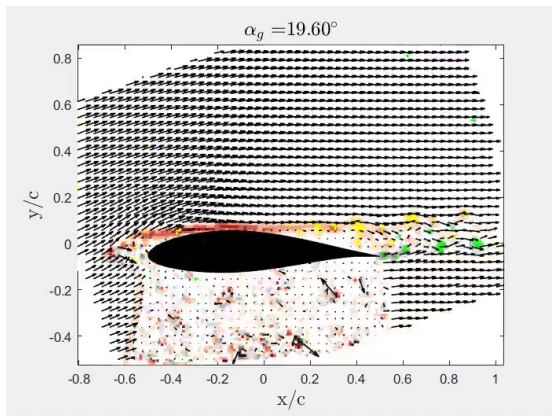
- 3) Vortex detection criterion :

- yellow circles : clockwise rotating vortices ( $\Gamma_2 > 0.7$ )
- green circles : counter-clockwise rotating vortices ( $\Gamma_2 < -0.7$ )

# Flow topology for $k = 0.05$ (dynamic regime)

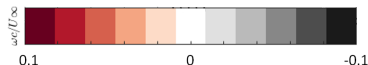
## Vortex detection criterion $\Gamma_2$

$$\Gamma_2(P) = \frac{1}{N} \sum_S \frac{[\underline{PM} \wedge (\underline{U}_M - \underline{U}_P)] \cdot \underline{z}}{\|\underline{PM}\| \cdot \|\underline{U}_M - \underline{U}_P\|} \quad \text{with } N = 3$$



## Flow evolution in the **airfoil reference system**

- 1) Streamlines
- 2) Normalized vorticity  $\omega c/U_\infty$  :



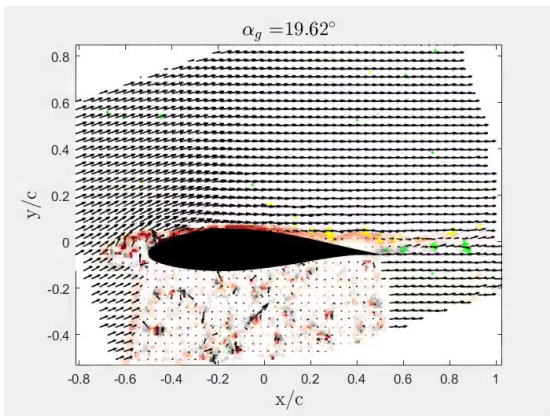
- 3) Vortex detection criterion :

- yellow circles : clockwise rotating vortices ( $\Gamma_2 > 0.7$ )
- green circles : counter-clockwise rotating vortices ( $\Gamma_2 < -0.7$ )

# Flow topology for $k = 0.025$ (transition regime)

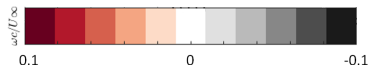
## Vortex detection criterion $\Gamma_2$

$$\Gamma_2(P) = \frac{1}{N} \sum_S \frac{[\underline{PM} \wedge (\underline{U}_M - \underline{U}_P)] \cdot \underline{z}}{\|\underline{PM}\| \cdot \|\underline{U}_M - \underline{U}_P\|} \quad \text{with } N = 3$$



## Flow evolution in the **airfoil reference system**

- 1) Streamlines
- 2) Normalized vorticity  $\omega c / U_\infty$  :

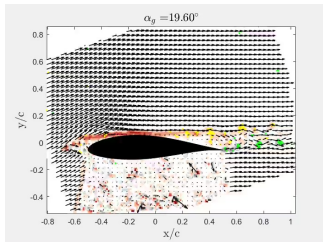


- 3) Vortex detection criterion :

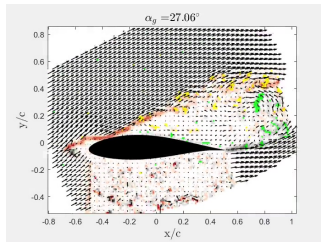
- yellow circles : clockwise rotating vortices ( $\Gamma_2 > 0.7$ )
- green circles : counter-clockwise rotating vortices ( $\Gamma_2 < -0.7$ )

# Snapshots for $k = 0.005$ (quasi-static regime)

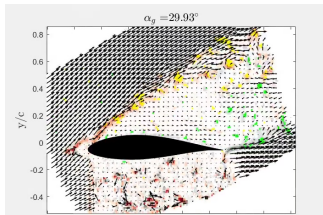
$$\alpha_g = 19.6^\circ$$



$$\alpha_g = 27^\circ$$

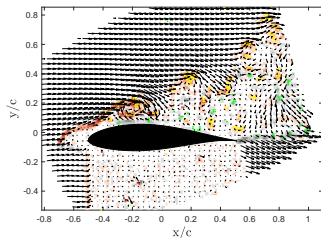


$$\alpha_g = 30^\circ$$

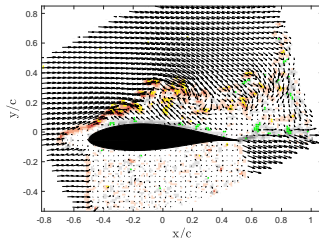


Flow topology at  $\alpha_g = 27^\circ$  and  $30^\circ$   
close to what has been observed in  
static conditions

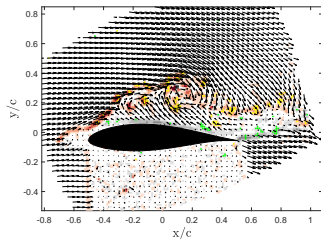
# Snapshots for $k = 0.05$ (dynamic regime)



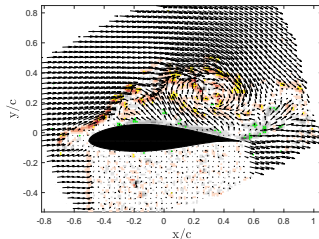
$$\alpha_g = 29.66^\circ \uparrow$$



$$\alpha_g = 29.85^\circ \uparrow$$



$$\alpha_g = 29.90^\circ \uparrow$$



$$\alpha_g = 29.97^\circ \uparrow$$

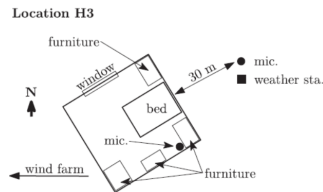
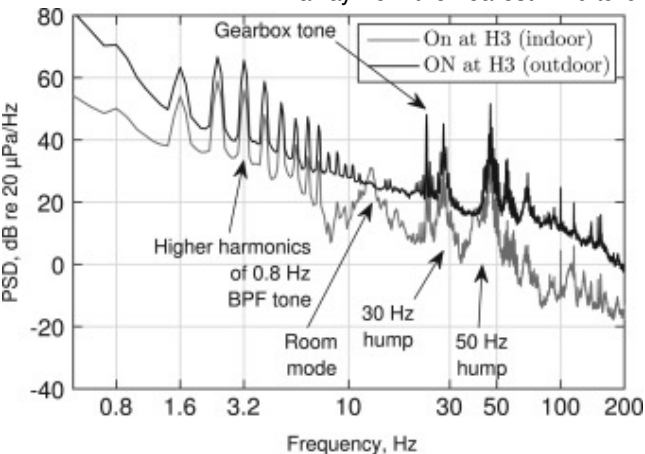
# Acknowledgments

This research has been funded by the French National Agency for Research under grant agreement N° ANR-19-CE36-0009



# Low frequency noise and infrasound

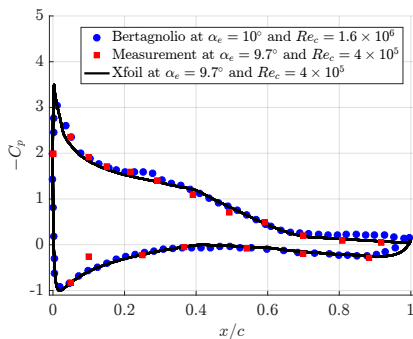
Indoor/outdoor power spectral densities measured by Zajamsek *et al.* (2016) 3 km away from the nearest wind turbine



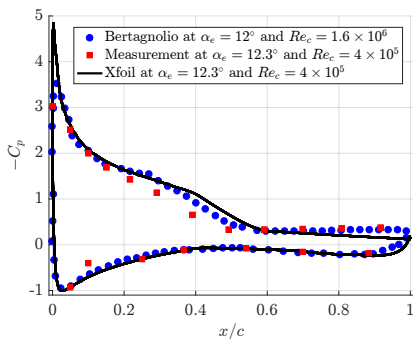


# Measurements for the NACA63<sub>3</sub>418 airfoil

Xfoil calculations using AoA corrections by Brooks *et al.* (1984) :  $\alpha_e \approx \alpha_g/1.55$



(a)  $\alpha_e \approx 10^\circ$



(b)  $\alpha_e \approx 12^\circ$

**FIGURE** – Pressure coefficient distribution measured by Bertagnolio *et al.* (2017) at  $Re_c = 1.6 \times 10^6$ , measured in the ECL anechoic wind tunnel at  $Re_c = 4 \times 10^5$ , and calculated with Xfoil at  $Re_c = 4 \times 10^5$ .